A dynamic variable (degree of freedom) is added.

Andersen: $\vec{r}_i = V^{1/3}\vec{\xi}_i \quad \dot{\vec{r}}_i = V^{1/3}\dot{\vec{\xi}}_i$

NO: $\dot{\vec{r}}_i \overset{?}{=} d\vec{r}_i/dt = d(V^{1/3}\vec{\xi}_i)/dt = \dot{V}V^{-2/3}\vec{\xi}_i/3 + V^{1/3}\dot{\vec{\xi}}_i$

Lagrangian $\mathcal{L} = \mathcal{L}(\vec{\xi}^N, \dot{\vec{\xi}}^N, V, \dot{V})$:

$$\mathcal{L} = \frac{1}{2}\sum_{i=1}^{N} m_i(V^{1/3}\dot{\vec{\xi}}_i)^2 + \frac{1}{2}M_V\dot{V}^2 - U(V^{1/3}\vec{\xi}^N) - PV$$

pressure $P \downarrow$
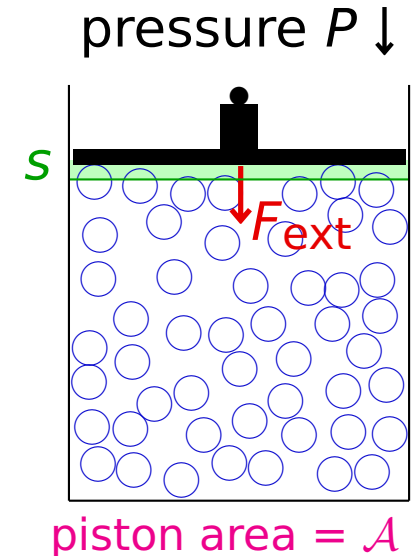
s

$\downarrow F_\text{ext}$

piston area $= \mathcal{A}$

Lagrange equations:

$$\frac{d}{dt}\left(\frac{\partial\mathcal{L}}{\partial\dot{q}}\right) = \frac{\partial\mathcal{L}}{\partial q}$$

Equations of motion:

$$M_V\ddot{V} = \frac{1}{3V}\left(\sum_{i=1}^{N}\vec{r}_i\cdot\vec{f}_i + 2E_\text{kin}\right) - P \equiv P_\text{cfg} - P$$

$$V^{1/3}\ddot{\vec{\xi}}_i = \frac{\vec{f}_i}{m_i}, \quad \text{back in real variables: } \ddot{\vec{r}}_i = \frac{d}{dt}V^{1/3}\dot{\vec{\xi}} = \frac{\vec{f}_i}{m_i} + \frac{\dot{V}\dot{\vec{r}}_i}{3V}$$

The Hamiltonian of the extended system is preserved:

canonically conjugate momentum p

$$\mathcal{H} = \sum_q \dot{q}\frac{\partial \mathcal{L}}{\partial \dot{q}} - \mathcal{L} = \frac{1}{2}\sum_{i=1}^{N}\frac{p^2}{V^{2/3}m_i} + \frac{1}{2}\frac{p_V^2}{M_V} + U(V^{1/3}\vec{\xi}^N) + PV$$

$$\equiv E_{\text{kin}} + E_{\text{kin. piston}} + E_{\text{pot}} + PV$$

Other methods:

- generalization (for crystals): Parrinello–Rahman

- Berendsen (friction) method (thermostat required because of dissipation)

$$\dot{V} = -\text{const} \times (P_{\text{cfg}} - P)$$

- Constraint dynamics

$$P = P_{\text{cfg}}(\vec{\xi}^N, \dot{\vec{\xi}}^N, V, \dot{V})$$

Nosé originally proposed:

$$\mathcal{L} = \sum_{i=1}^{N} \frac{m_i}{2} s^2 \dot{\vec{r}}_i'^2 - U(\vec{r}'^N) + \frac{M_s}{2}\dot{s}^2 - f' k_B T \ln s$$

"Rescaling of the kinetic energy by means of velocity, $\dot{\vec{r}} = s\dot{\vec{r}}'$; the scaling degree of freedom s has a kinetic as well as potential energy"

Equations of motion (why we write t': see below)

$$\frac{d}{dt'}(m_i s^2 \dot{\vec{r}}_i') = \vec{f}_i$$

$$M_s \frac{d^2 s}{dt'^2} = \sum_{i=1}^{N} m_i s \dot{\vec{r}}_i'^2 - \frac{f' k_B T}{s}$$

Hamiltonian

$$\mathcal{H} = \sum_{i=1}^{N} \frac{\vec{p}_i'^2}{2 m_i s^2} + U(\vec{r}'^N) + \frac{p_s'^2}{2 M_s} + f' k_B T \ln s$$

Canonically conjugate impulses (momenta):

$$\vec{p}_i' = \frac{\partial \mathcal{L}}{\partial \dot{\vec{r}}_i} = m_i s^2 \dot{\vec{r}}_i', \qquad p_s' = \frac{\partial \mathcal{L}}{\partial \dot{s}} = M_s \dot{s}$$

Nosé: For $f' =$ # of degrees of freedom incl. s we get the canonical distribution od static variables (but see below...)
N particles in a general conservative field: $f' = 3N + 1$

Problems: correct velocity is $\dot{\vec{r}}_i = s\dot{\vec{r}}'_i$, so if s changes a lot, the integration step should change accordingly

Hoover: $\dot{\vec{r}}_i = s\dot{\vec{r}}'_i$ is the same as time rescaling, $\dot{\vec{r}}_i = s\mathrm{d}\vec{r}_i/\mathrm{d}t'$, i.e.:

$$s\,\mathrm{d}t = \mathrm{d}t' \quad \text{or} \quad \frac{\mathrm{d}}{\mathrm{d}t'} = \frac{1}{s}\frac{\mathrm{d}}{\mathrm{d}t}$$

this trick brings us back to the physical (unscaled) velocities and momenta:

$$\vec{r}_i = \vec{r}'_i, \qquad \dot{\vec{r}}_i \equiv \frac{\mathrm{d}\vec{r}_i}{\mathrm{d}t} = s\frac{\mathrm{d}\vec{r}_i}{\mathrm{d}t'} \equiv s\dot{\vec{r}}'_i, \qquad \vec{p}_i = \vec{p}'_i/s, \qquad p_s = p'_s/s$$

Equations of motion:

$$m_i \frac{1}{s}\frac{\mathrm{d}}{\mathrm{d}t} s\dot{\vec{r}}_i = \frac{m_i}{s}[\dot{s}\dot{\vec{r}}_i + s\ddot{\vec{r}}] = \vec{f}_i$$

$$M_s \frac{1}{s}\frac{\mathrm{d}}{\mathrm{d}t}\frac{1}{s}\frac{\mathrm{d}}{\mathrm{d}t}s = \frac{M_s}{s}\left[\left(\frac{\ddot{s}}{s}\right) - \left(\frac{\dot{s}}{s}\right)^2\right] = \frac{1}{s}\left(\sum_{i=1}^{N} m_i\dot{\vec{r}}_i^2 - fk_\mathrm{B}T\right)$$

Another trick: substitution $\xi = \ln s$. Then:

$$\ddot{\vec{r}}_i = \frac{\vec{f}_i}{m_i} - \dot{\vec{r}}_i \dot{\xi}$$

$$\ddot{\xi} = \left(\frac{T_{\text{kin}}}{T} - 1\right)\tau^{-2}$$

time constant of the thermostat:

$$\tau = \sqrt{\frac{M_s}{f k_{\text{B}} T}}$$

Conserved quantity (not a Hamiltonian because not a function of coordinates and conjugate momenta), can be proven by taking a derivative:

$$E_{\text{Nosé–Hoover}} = \sum_{i=1}^{N} \frac{1}{2} m_i \dot{r}_i^2 + U + f k_{\text{B}} T \left[\xi + \frac{\tau^2 \dot{\xi}^2}{2}\right] = \text{const}$$
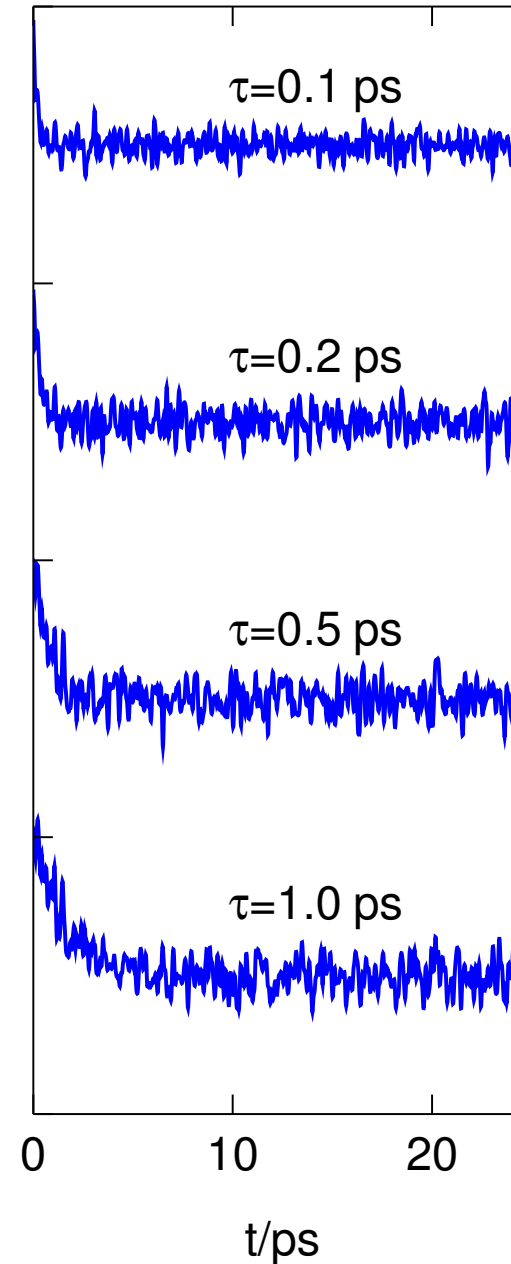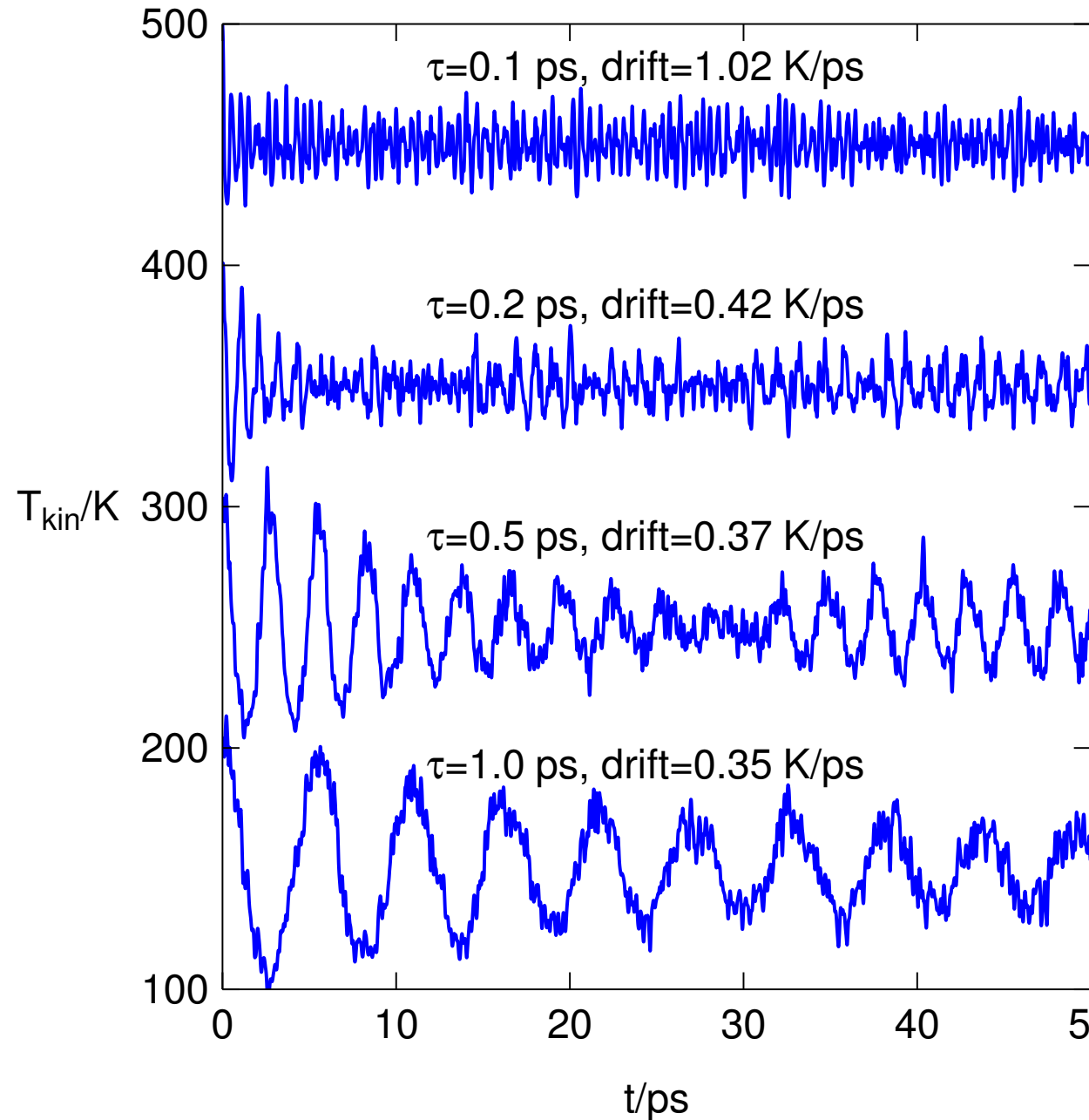
Hoover showed that these equations give the canonical distribution if f is the number of degrees of freedom (without ξ or s)
N particles in a general conservative field: $f = 3N$

T_{kin}/K

τ=0.1 ps, drift=1.02 K/ps

τ=0.2 ps, drift=0.42 K/ps

τ=0.5 ps, drift=0.37 K/ps

τ=1.0 ps, drift=0.35 K/ps

τ=0.1 ps

τ=0.2 ps

τ=0.5 ps

τ=1.0 ps

t/ps

t/ps

Problem of time scaling ($\dot{r} = s\dot{r}'$, i.e., $\mathrm{d}t = \mathrm{d}t'/s$)

$$\langle A \rangle = \frac{\int_{t_0}^{t_1} A(t)\mathrm{d}t}{\int_{t_0}^{t_1} \mathrm{d}t} = \frac{\int_{t_0}^{t_1} A(t)\mathrm{d}t'/s}{\int_{t_0}^{t_1} \mathrm{d}t'/s} = \frac{\langle A/s \rangle'}{\langle 1/s \rangle'}$$

The expectation value for $\mathcal{H} = E$:

$$\langle A \rangle = \frac{\langle A/s \rangle'}{\langle 1/s \rangle'} = \frac{\int \frac{A}{s}\mathrm{d}p_s'\mathrm{d}\vec{p}'^N \mathrm{d}s\mathrm{d}\vec{r}^N \delta(\mathcal{H} - E)}{\int \frac{1}{s}\mathrm{d}p_s'\mathrm{d}\vec{p}'^N \mathrm{d}s\mathrm{d}\vec{r}^N \delta(\mathcal{H} - E)}$$

Trick: We will integrate over $\vec{p}$, not $\vec{p}'$.

After transformation $\mathrm{d}\vec{p}'_i = s^3\mathrm{d}\vec{p}_i$ we get:

$$\langle A \rangle = \frac{\displaystyle\int A s^{f-1}\mathrm{d}p'_s\mathrm{d}\vec{p}^N\mathrm{d}s\mathrm{d}\vec{r}^N\delta\left(\mathcal{H}_0 + \frac{p'^2_s}{2M_s} + fk_\mathrm{B}T\ln s - E\right)}{\displaystyle\int s^{f-1}\mathrm{d}p'_s\mathrm{d}\vec{p}^N\mathrm{d}s\mathrm{d}\vec{r}^N\delta\left(\mathcal{H}_0 + \frac{p'^2_s}{2M_s} + fk_\mathrm{B}T\ln s - E\right)}$$

Where we have donoted

$$\mathcal{H}_0(\vec{p}^N, \vec{r}^N) = \sum_{i=1}^{N}\frac{\vec{p}^2_i}{2m_i} + U(\vec{r}^N)$$

and where the number of degrees of freedom is $f = 3N$.
(If a quantity like the total momentum is conserved, a substitution must be used.)

We will integrate over s first. We shall use the formula:

$$\delta(F(s)) = \sum_{s_0, F(s_0)=0} \frac{\delta(s-s_0)}{|F'(s_0)|}$$

So we need all roots of the argument of $\delta()$; there is only one:

$$s_0 = \exp\left[-\frac{1}{fk_BT}\left(\mathcal{H}_0 + \frac{p_s'^2}{2M_s} - E\right)\right], \qquad F'(s_0) = \frac{fk_BT}{s_0}$$

After integration:

$$\langle A \rangle = \frac{\displaystyle\int A\, dp_s'\, d\vec{p}^N\, d\vec{r}^N \exp\left[-\frac{f}{fk_BT}\left(\mathcal{H}_0 + \frac{p_s'^2}{2M_s} - E\right)\right]}{\displaystyle\int dp_s'\, d\vec{p}^N\, d\vec{r}^N \exp\left[-\frac{f}{fk_BT}\left(\mathcal{H}_0 + \frac{p_s'^2}{2M_s} - E\right)\right]}$$

The last integration is over $\mathrm{d}p'_s$. Many terms then cancel out:

$$\langle A \rangle = \frac{\displaystyle\int A\,\mathrm{d}\vec{p}^N\mathrm{d}\vec{r}^N \exp(-\mathcal{H}_0/k_\mathrm{B}T)}{\displaystyle\int \mathrm{d}\vec{p}^N\mathrm{d}\vec{r}^N \exp(-\mathcal{H}_0/k_\mathrm{B}T)}, \quad \text{q.e.d}$$

Exercise: thermostats +

⬤ Simulate liquid water SPC/E and compare the following thermostats:
  – Berendsen
  – Nosé-Hoover
  – Andersen (for the center of mass)
  – Maxwell (for the center of mass)

The cutoff-electrostatics version cookce is recommended (it is faster than Ewald)

The needed files are in /home/guest/termostaty.zip:

```
guest@403-a324-01:~/VY$ unzip ../termostaty.zip
```
spce.ble = force field definition of SPC/E
water.def = commented simulation parameters

⬤ To start simulation, use the Berensen thermostat and the default method Verlet+Shake:
```
guest@403-a324-01:~/VY$ cookce spce water -s
thermostat="Berendsen"
init="crystal"
```
Stop the simulation by pressing ctrl-C at temperature around 500 K

⬤ Now try various thermostats (`-w0` prevents writing the final configuration):
```
guest@403-a324-01:~/VY$ cookce spce water -s -w0
tau.T=...
thermostat="..."
```

Nosé–Hoover combined with Verlet+Shake uses a velocity predictor (there are other methods, too)

You may try also the Gear integration combined with the Berendsen and Nosé–Hoover thermostat (Gear 4th order = option `-m4`), e.g.:
```
guest@403-a324-01:~/VY$ cookce spce water -m4 -s -w0
thermostat="Nose-Hoover"
```

The Gear integration is less accurate with `thermostat="Andersen"` and `"Maxwell"` (higher-order terms are not accurate)

⬤ After a few ps run look at the convergence profile of temperatures:
```
guest@403-a324-01:~/VY$ showcp -p water Tkin
```
(white = total T_{kin}, yellow = rotational, cyan = translational)