# **Extended Lagrangian methods in MD: NPT**

 $+\frac{1/12}{511/3}$ 

A dynamic variable (degree of freedom) is added.

Andersen:  $\vec{r}_i = V^{1/3} \vec{\xi}_i$   $\vec{r}_i = V^{1/3} \vec{\xi}_i$ 

NO:  $\dot{\vec{r}}_i \stackrel{?}{=} d\vec{r}_i/dt = d(V^{1/3}\vec{\xi}_i)/dt = \dot{V}V^{-2/3}\vec{\xi}_i/3 + V^{1/3}\dot{\vec{\xi}}_i$ 

Lagrangian  $\mathcal{L} = \mathcal{L}(\vec{\xi}^N, \dot{\vec{\xi}}^N, V, \dot{V})$ :

$$\mathcal{L} = \frac{1}{2} \sum_{i=1}^{N} m_i (V^{1/3} \dot{\xi}_i)^2 + \frac{1}{2} M_V \dot{V}^2 - U(V^{1/3} \dot{\xi}^N) - PV$$

Lagrange equations:

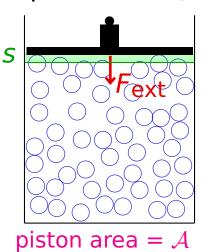
$$\frac{\mathsf{d}}{\mathsf{d}t} \left( \frac{\partial \mathcal{L}}{\partial \dot{q}} \right) = \frac{\partial \mathcal{L}}{\partial q}$$

Equations of motion:

$$M_V \ddot{V} = \frac{1}{3V} \left( \sum_{i=1}^N \vec{r}_i \cdot \vec{f}_i + 2E_{\text{kin}} \right) - P \equiv P_{\text{cfg}} - P$$

$$V^{1/3}\ddot{\xi}_i = \frac{\vec{f}_i}{m_i}$$
, back in real variables:  $\ddot{r}_i = \frac{d}{dt}V^{1/3}\dot{\xi} = \frac{\vec{f}_i}{m_i} + \frac{\dot{V}\dot{r}_i}{3V}$ 

pressure *P* ↓



# **Extended Lagrangian methods in MD: NPT**

 $+\frac{2/12}{s11/3}$ 

The Hamiltonian of the extended system is preserved:

canonically conjugate momentum p

$$\mathcal{H} = \sum_{q} \dot{q} \frac{\partial \mathcal{L}}{\partial \dot{q}} - \mathcal{L} = \frac{1}{2} \sum_{i=1}^{N} \frac{p^2}{V^{2/3} m_i} + \frac{1}{2} \frac{p_V^2}{M_V} + U(V^{1/3} \vec{\xi}^N) + PV$$

$$\equiv E_{\text{kin}} + E_{\text{kin. piston}} + E_{\text{pot}} + PV$$

#### Other methods:

- generalization (for crystals): Parrinello-Rahman
- Berendsen (friction) method (thermostat required because of dissipation)

$$\dot{V} = -\text{const} \times (P_{\text{cfg}} - P)$$

Constraint dynamics

$$P = P_{\text{cfg}}(\vec{\xi}^N, \dot{\vec{\xi}}^N, V, \dot{V})$$

**Nosé** originally proposed:

$$\mathcal{L} = \sum_{i=1}^{N} \frac{m_i}{2} s^2 \dot{\vec{r}}_i'^2 - U(\vec{r}'^N) + \frac{M_s}{2} \dot{s}^2 - f' k_B T \ln s$$

"Rescaling of the kinetic energy by means of velocity,  $\dot{\vec{r}} = s\dot{\vec{r}}'$ ; the scaling degree of freedom s has a kinetic as well as potential energy"

Equations of motion (why we write t': see below)

$$\frac{d}{dt'}(m_i s^2 \dot{\vec{r}}_i') = \vec{f}_i$$

$$M_s \frac{d^2 s}{dt'^2} = \sum_{i=1}^N m_i s \dot{\vec{r}}_i'^2 - \frac{f' k_B T}{s}$$

Hamiltonian

$$\mathcal{H} = \sum_{i=1}^{N} \frac{\vec{p}_{i}^{\prime 2}}{2m_{i}s^{2}} + U(\vec{r}^{\prime N}) + \frac{p_{s}^{\prime 2}}{2M_{s}} + f^{\prime}k_{B}T \ln s$$

Canonically conjugate impulses (momenta):

$$\vec{p}'_i = \frac{\partial \mathcal{L}}{\partial \dot{\vec{r}}_i} = m_i s^2 \dot{\vec{r}}'_i, \qquad p'_s = \frac{\partial \mathcal{L}}{\partial \dot{s}} = M_s \dot{s}$$

## **Nosé-Hoover thermostat**

 $+\frac{4/12}{s11/3}$ 

**Nosé:** For f' = # of degrees of freedom incl. s we get the canonical distribution od static variables (but see below...)

N particles in a general conservative field: f' = 3N + 1

**Problems:** correct velocity is  $\dot{\vec{r}}_i = s\dot{\vec{r}}_i'$ , so if s changes a lot, the integration step should change accordingly

**Hoover:**  $\dot{\vec{r}}_i = s\dot{\vec{r}}_i'$  is the same as time rescaling,  $\dot{\vec{r}}_i = sd\vec{r}_i/dt'$ , i.e.:

$$sdt = dt'$$
 or  $\frac{d}{dt'} = \frac{1}{s} \frac{d}{dt}$ 

this trick brings us back to the physical (unscaled) velocities and momenta:

$$\vec{r}_i = \vec{r}'_i$$
,  $\dot{\vec{r}}_i \equiv \frac{d\vec{r}_i}{dt} = s \frac{d\vec{r}_i}{dt'} \equiv s \dot{\vec{r}}'_i$ ,  $\vec{p}_i = \vec{p}'_i/s$ ,  $p_s = p'_s/s$ 

Equations of motion:

$$m_{i} \frac{1}{s} \frac{d}{dt} s \dot{\vec{r}}_{i} = \frac{m_{i}}{s} [\dot{s} \dot{\vec{r}}_{i} + s \ddot{\vec{r}}] = \vec{f}_{i}$$

$$M_{s} \frac{1}{s} \frac{d}{dt} \frac{1}{s} \frac{d}{dt} s = \frac{M_{s}}{s} \left[ \left( \frac{\ddot{s}}{s} \right) - \left( \frac{\dot{s}}{s} \right)^{2} \right] = \frac{1}{s} \left( \sum_{i=1}^{N} m_{i} \dot{\vec{r}}_{i}^{2} - f k_{B} T \right)$$

#### **Nosé-Hoover thermostat**

 $+\frac{5/12}{511/3}$ 

Another trick: substitution  $\xi = \ln s$ . Then:

$$\ddot{\vec{r}}_{l} = \frac{\vec{f}_{l}}{m_{l}} - \dot{\vec{r}}_{l} \dot{\xi}$$

$$\ddot{\xi} = \left(\frac{T_{kin}}{T} - 1\right) \tau^{-2}$$

time constant of the thermostat:

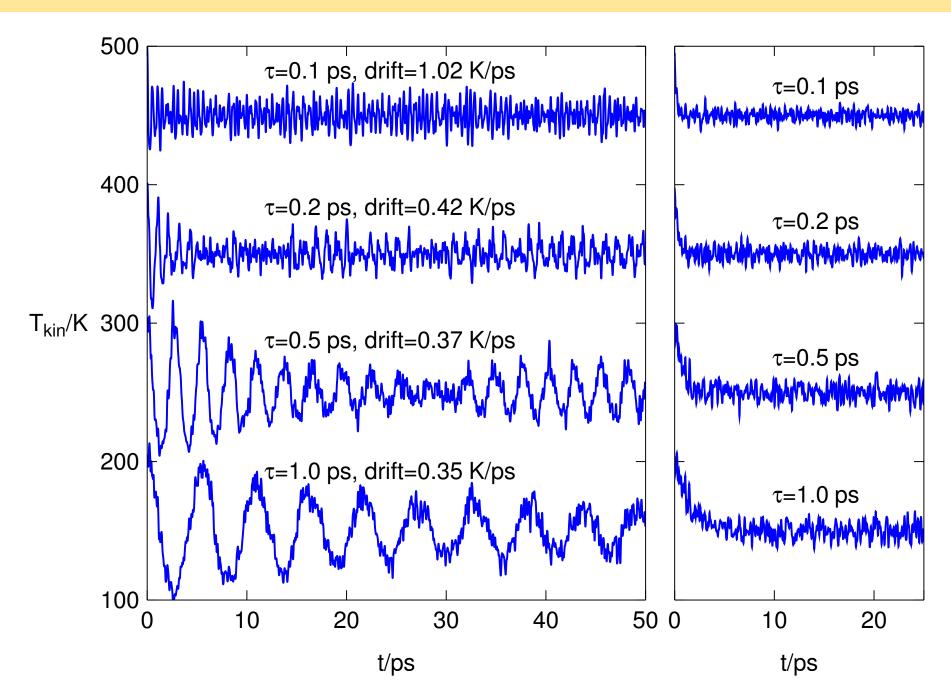
$$\tau = \sqrt{\frac{M_S}{fk_BT}}$$

Conserved quantity (not a Hamiltonian because not a function of coordinates and conjugate momenta), can be proven by taking a derivateve:

$$E_{\text{Nosé-Hoover}} = \sum_{i=1}^{N} \frac{1}{2} m_i \dot{r}_i^2 + U + f k_{\text{B}} T \left| \xi + \frac{\tau^2 \dot{\xi}^2}{2} \right| = \text{const}$$

Hoover showed that these equations give the canonical distribution if f is the number of degrees of freedom (without  $\xi$  or s)

N particles in a general conservative field: f = 3N



### Nosé-Hoover derivation I

Problem of time scaling  $(\dot{r} = s\dot{r}', i.e., dt = dt'/s)$ 

$$\langle A \rangle = \frac{\int_{t_0}^{t_1} A(t) dt}{\int_{t_0}^{t_1} dt} = \frac{\int_{t_0}^{t_1} A(t) dt'/s}{\int_{t_0}^{t_1} dt'/s} = \frac{\langle A/s \rangle'}{\langle 1/s \rangle'}$$

The expectation value for  $\mathcal{H} = E$ :

$$\langle A \rangle = \frac{\langle A/s \rangle'}{\langle 1/s \rangle'} = \frac{\int \frac{A}{s} dp'_{s} d\vec{p}'^{N} ds d\vec{r}^{N} \delta (\mathcal{H} - E)}{\int \frac{1}{s} dp'_{s} d\vec{p}'^{N} ds d\vec{r}^{N} \delta (\mathcal{H} - E)}$$

Trick: We will integrate over  $\vec{p}$ , not  $\vec{p}'$ .

After transformation  $d\vec{p}'_i = s^3 d\vec{p}_i$  we get:

$$\langle A \rangle = \frac{\int A s^{f-1} \mathrm{d} p_s' \mathrm{d} \vec{p}^N \mathrm{d} s \mathrm{d} \vec{r}^N \delta \left( \mathcal{H}_0 + \frac{p_s'^2}{2M_s} + f k_\mathrm{B} T \ln s - E \right)}{\int s^{f-1} \mathrm{d} p_s' \mathrm{d} \vec{p}^N \mathrm{d} s \mathrm{d} \vec{r}^N \delta \left( \mathcal{H}_0 + \frac{p_s'^2}{2M_s} + f k_\mathrm{B} T \ln s - E \right)}$$

Where we have donoted

$$\mathcal{H}_0(\vec{p}^N, \vec{r}^N) = \sum_{i=1}^N \frac{\vec{p}_i^2}{2m_i} + U(\vec{r}^N)$$

and where the number of degrees of freedom is f = 3N.

(If a quantity like the total momentum is conserved, a substitution must be used.)

We will integrate over *s* first. We shall use the formula:

$$\delta(F(s)) = \sum_{s_0, F(s_0) = 0} \frac{\delta(s - s_0)}{|F'(s_0)|}$$

So we need all roots of the argument of  $\delta()$ ; there is only one:

$$s_0 = \exp \left[ -\frac{1}{fk_BT} \left( \mathcal{H}_0 + \frac{p_s'^2}{2M_s} - E \right) \right], \qquad F'(s_0) = \frac{fk_BT}{s_0}$$

After integration:

$$\langle A \rangle = \frac{\int A dp'_{S} d\vec{p}^{N} d\vec{r}^{N} \exp \left[ -\frac{f}{fk_{B}T} \left( \mathcal{H}_{0} + \frac{p'_{S}^{2}}{2M_{S}} - E \right) \right]}{\int dp'_{S} d\vec{p}^{N} d\vec{r}^{N} \exp \left[ -\frac{f}{fk_{B}T} \left( \mathcal{H}_{0} + \frac{p'_{S}^{2}}{2M_{S}} - E \right) \right]}$$

### Nosé-Hoover derivation IV

The last integration is over  $dp'_s$ . Many terms then cancel out:

$$\langle A \rangle = \frac{\int A d\vec{p}^N d\vec{r}^N \exp(-\mathcal{H}_0/k_B T)}{\int d\vec{p}^N d\vec{r}^N \exp(-\mathcal{H}_0/k_B T)}, \quad \text{q.e.d}$$

- Simulate liquid water SPC/E and compare the following thermostats:
  - Berendsen
  - Nosé-Hoover
  - Andersen (for the center of mass)
  - Maxwell (for the center of mass)

The cutoff-electrostatics version cookce is recommended (it is faster than Ewald)

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The needed files are in /home/guest/termostaty.zip:
guest@403-a324-01:~/VY$ unzip ../termostaty.zip
spce.ble = force field definition of SPC/E
water.def = commented simulation parameters
```

■ To start simulation, use the Berensen thermostat and the default method Verlet+Shake: guest@403-a324-01:~/VY\$ cookce spce water -s thermostat="Berendsen" init="crystal"

Stop the simulation by pressing ctrl-C at temperature around 500 K

Now try various thermostats (-w0 prevents writing the final configuration): guest@403-a324-01:~/VY\$ cookce spce water -s -w0 tau.T=... thermostat="..."

Nosé-Hoover combined with Verlet+Shake uses a velocity predictor (there are other methods, too)

You may try also the Gear integration combined with the Berendsen and Nosé-Hoover thermostat (Gear 4th order = option -m4), e.g.:

guest@403-a324-01:~/VY\$ cookce spce water -m4 -s -w0
thermostat="Nose-Hoover"

The Gear integration is less accurate with thermostat="Andersen" and "Maxwell" (higher-order terms are not accurate)

After a few ps run look at the convergence profile of temperatures:  $guest@403-a324-01:\sim/VY$$  showcp -p water Tkin (white = total  $T_{kin}$ , yellow = rotational, cyan = translational)